# 自由曲面の製造 Manufacturing of free-form optics

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## Introduction: Potential of Free-form Optics





Conventional Optical Design Korsch FoV  $\sim \Phi 1 \deg$ 

Three Mirror Anastigmat TMA (designed by us) FoV  $\sim \Phi 4 \deg$ 

## Introduction

# Limitation of Interferometer

- Interferometer is a powerful tool for a test of optics.
  - requiring an accurate and custom-made reference surface (null optics)
  - requiring a stable and large space equivalent to the radius of curvature (RoC) of the test mirror
  - challenging to test a large flat, and convex surface nearly impossible to test free-form optics highly aspheric



### Introduction Limitation of CMM/Mechanical method

- Coordinate measurement machine is a powerful tool for testing free-form optics.
  - limited to size up to 1 m
  - very few tools which can both test and polish



## Three Point Method (TPM)



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- Three-sensor unit travels with linear guide
- Sag or hump (local curvature) is obtained with 2s<sub>2</sub>-s<sub>1</sub>-s<sub>3</sub>
- Local curvatures are doubly integrated along the scanning path
- The cross-sectional shape of the test surface is obtained
- Measuring local curvature is insensitive to motion error of the unit
- Precise reference (null optics) is not required → Free-form
  ⊗
- Low spatial resolution
- Sensor noise is also magnified with the integration process.
- Inapplicable to surface departing from flat

## Dragging TPM



- Dragging TPM drags a probe unit on the test surface.
  - Difference of the local curvature from the design value is integrated along the path for obtaining the figure error.

Dragging TPM

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A linear guide is not required. A large measurement range of sensors is not required. Resistant to temperature changes and vibration It can be mounted on a polishing machine. →Measurable range is not limited

## Robot Arm System

- Polish & Profilometer
- Work Area: φ1.8m
- Small space
- Robust
- Cost saving





#### Polish

#### Measurement

## Data Stitching Algorithm

- Sensor error is emphasized with the integral procedure.
- The cross-sectional data is inconsistent with each other at the intersection after least squares.
- New algorithm deals with the data as a deformable *linear elastic body* and stitches the data without inconsistency.
- The solver is based on FEM (minimum energy).



Image of stitching elastic bodies

### Simulation



Raw data is made using a three-point method with a sensor noise of 1 nm and 100 steps. Raw data has inconsistencies at the intersections and has a discontinuous surface. Stitched surface reduces figure error and has a continuous surface. The circle path at the edge dramatically improves the figure error.

## Repeatability on flat mirror

0201-2

0203-1

0201-1

0202-2

1 m



Polishing flat mirror



Motion of robot-arm and table

-0.3 um

6 times measurements RMS < 10 nm 0.3 um

0202-1

0203-2

### Convex Aspheric



P-V = 2,400 nm RMS = 550 nm After grinding



RMS = 350 nm

6/14



1 m

RMS = 150 nm 6/15



RMS = 130 nm

RMS = 35 nm

### Seimei Telescope



Flat mirror



Seimei 3.8 m telescope The largest telescope in East-Asia



Convex Aspheric





### Hartmann Test





### Current and Future Work

- 2-m off axis parabola
  - Telescope for observing planets in our solar system
- Three mirror anastigmat (TMA) telescope
  - 0.5 m aperture
  - FoV of Φ4 deg
  - Off-axis and good MTF



2-m off axis parabola for PLANETS



### Conclusion

- We developed new manufacturing system for free form and one-meter scale optics.
- The system figured out the M2 and M3 mirrors of Seimei telescope.
- The system finished 1m convex M2 within one month with the figure error of 35 nm RMS.
- We confirmed the optical performance of M2 and M3 with the Shack Hartmann test and obtained the Hartmann constant of 0".26.